

## DESIGN OF A THRESHOLD AUTOMATIC COMPENSATION CIRCUIT FOR A VOLTAGE CONTROLLED OSCILLATOR USING A SCHMITT-TRIGGER CIRCUIT WITH CMOS INVERTERS

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**ABSTRACT.** *A voltage controlled oscillator (VCO) is an important circuit which is applied for phase locked loop (PLL) and various measuring devices. When we constitute the VCO based on the Miller integrator and the Schmitt-trigger circuit with operational amplifiers, the VCO has a problem that the relation between the oscillating frequency and the control voltage does not agree with the theoretical value by the delay of the operational amplifier. To solve this problem, we have already proposed the VCO using the Schmitt-trigger circuit with complementary metal-oxide-semiconductor (CMOS) inverters. However, the variation of the threshold voltage of the CMOS inverter affects the direct current (DC) component of the triangular wave. In this paper, we propose a VCO using a novel threshold automatic compensation circuit. Owing to the threshold automatic compensation circuit, the proposed circuit can realize the triangular wave around 0V. Furthermore, feasibility and effectiveness of the proposed circuit are demonstrated through the experiment using fabricated integrated circuit (IC) chips.*

**Keywords:** VCO, Schmitt-trigger, CMOS inverter, Miller integrator

**1. Introduction.** A voltage controlled oscillator (VCO) is an important circuit which is applied for phase locked loops (PLLs) and various measuring devices, and it has various types [1-5]. When the VCO is designed in a simplified form, operational amplifiers or CMOS logic gates are generally used. However, a parameter that determines the oscillating frequency includes the threshold voltage when the complementary metal-oxide-semiconductor (CMOS) logic gate is employed. For this reason, the VCO has a problem that the oscillating frequency is varied by ambient temperature and so on [6].

On the other hand, the reversal level of the circuit operation is decided by external resistances regardless of ambient temperature when the operational amplifier is employed. Therefore, in this case, the VCO can achieve the stable operation [7]. However, the output of a triangular wave increases higher than the setting voltage when the Schmitt-trigger circuit is constituted by the operational amplifier. As a result, the VCO has a problem that the relation between the oscillating frequency and the control voltage does not agree with the theoretical value by the delay of the operational amplifier. To solve this problem, we have already proposed the VCO using the Miller integrator with an operational amplifier

and the Schmitt-trigger circuit with CMOS inverters [8]. The VCO reported in [8] is less affected by the delay of circuit elements as the Schmitt-trigger circuit is constituted by using CMOS inverters even when the oscillating frequency is high. Therefore, the relation between the control voltage and the oscillating frequency shows good linearity in this VCO. Furthermore, by adding a threshold automatic compensation circuit to the VCO, the threshold voltage of the CMOS inverter can be kept at 0V automatically. Therefore, the direct current (DC) component of the triangular wave is not affected by the variation of the threshold voltage of the CMOS inverter.

In this paper, we propose a VCO using a novel threshold automatic compensation circuit. Owing to the threshold automatic compensation circuit, the proposed circuit can realize the triangular wave around 0V. Furthermore, in the relationship between the control voltage and the oscillating frequency, the proposed circuit shows better linearity than the conventional circuit. Concerning fabricated integrated circuit (IC) chips of the proposed circuit, the characteristics of the proposed circuit are clarified.

**2. Circuit Configurations.** First, we describe the problem of the conventional VCO using the Miller integrator and the Schmitt-trigger circuit. Figure 1 shows the circuit configuration of the conventional VCO using the Miller integrator and the Schmitt-trigger circuit with an operational amplifier. This circuit converts the triangular wave of the Miller integrator into the rectangular pulse by utilizing the hysteresis characteristic of the Schmitt-trigger circuit that has the positive threshold  $V_H$  and the negative threshold  $V_L$ . Therefore, the amplitude of the triangular wave increases higher than the setting voltage when the oscillating frequency is high. As a result, the relation between the control voltage and the oscillating frequency does not agree with the theoretical value.

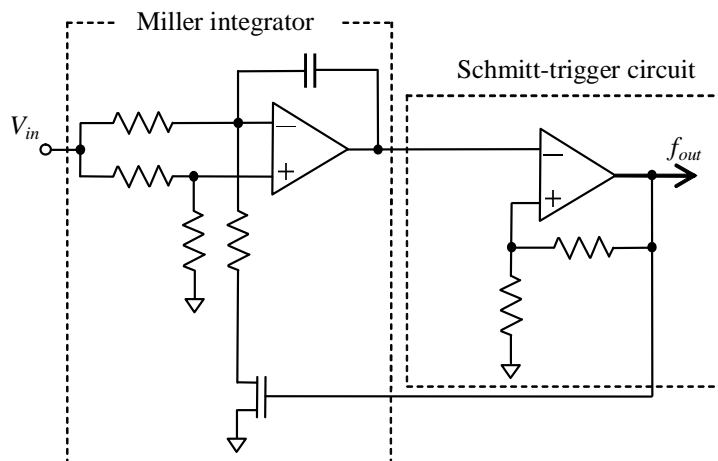


FIGURE 1. Circuit configuration of the conventional VCO based on the Miller integrator and the Schmitt-trigger circuit with the operational amplifier

Figure 2 shows the VCO which solves the delay of the operational amplifier by the Schmitt-trigger circuit using CMOS inverters. In this circuit, the variation of the threshold voltage of the CMOS inverter affects the DC component of the triangular wave. Therefore, it is difficult to realize the triangular wave around 0V. However, by adding a threshold automatic compensation circuit shown in Figure 3, we have already solved this problem in [8]. The VCO of Figure 3 can offer the triangular wave around 0V, because the threshold automatic compensation circuit is added to the source of n-MOS of the first CMOS inverter in the Schmitt-trigger circuit.

Figure 4 shows the circuit configuration of the proposed VCO with the threshold automatic compensation circuit using the Miller integrator with an operational amplifier

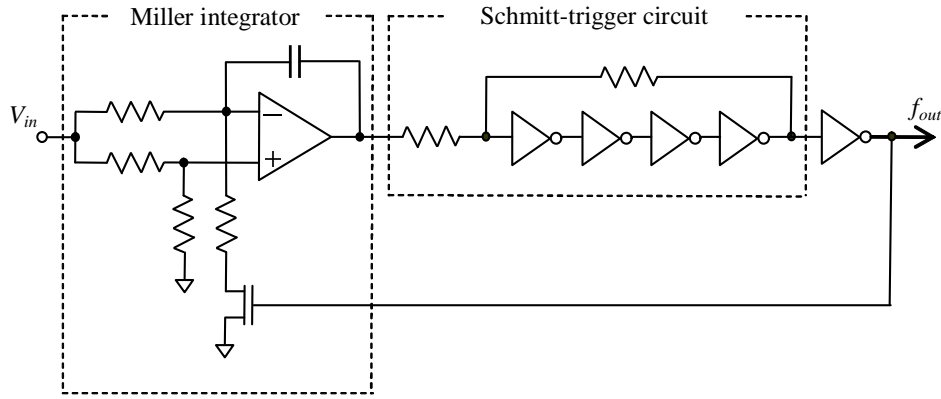


FIGURE 2. Circuit configuration of the conventional VCO based on the Schmitt-trigger circuit with CMOS inverters

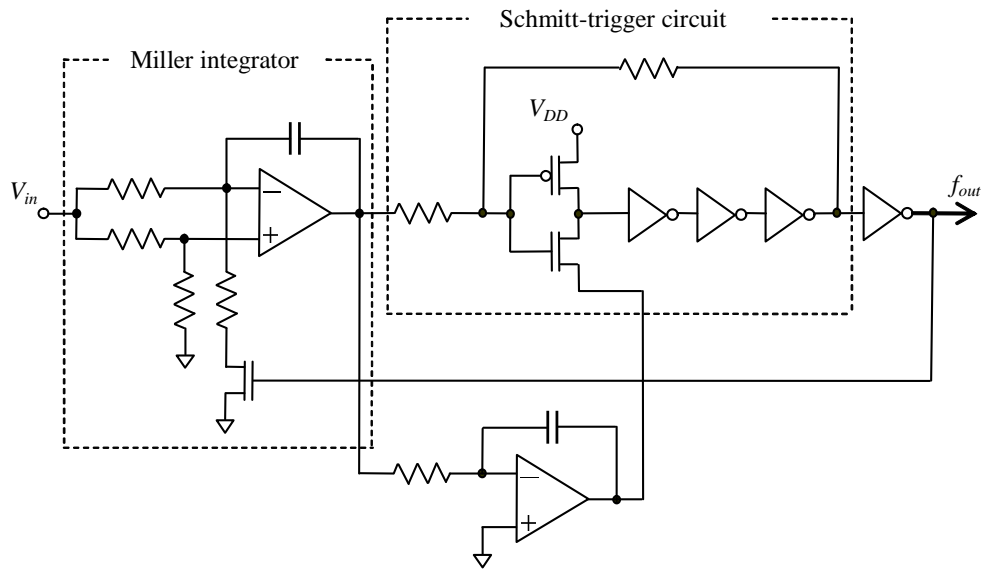


FIGURE 3. Circuit configuration of the conventional VCO with the threshold automatic compensation circuit

and the Schmitt-trigger circuit with CMOS inverters. In Figure 4,  $A_1$ ,  $R_1$ - $R_4$ , and  $C_1$  are an operational amplifier, resistances, and a capacitance for the Miller integrator, respectively.  $M_2$ ,  $M_3$ ,  $N_1$ - $N_3$ ,  $R_5$ ,  $R_6$  are MOS transistors, CMOS inverters, and resistances for the Schmitt-trigger circuit.  $N_4$  and  $M_1$  are the CMOS inverters to control the charge and discharge operation using the output of the Miller integrator and the MOS transistor which has the operation of the switch.  $A_2$ ,  $A_3$ ,  $M_4$ ,  $R_7$ - $R_9$ ,  $C_2$  are operational amplifiers, a MOS transistor, resistances, and a capacitance for the threshold automatic compensation circuit. The capacitance  $C_2$  of the threshold automatic compensation circuit is designed sufficiently bigger than the capacitance  $C_1$ .

### 3. Operation Analysis.

**3.1. Oscillating operation.** When the output of  $N_4$  is in a high level,  $M_1$  is turned “ON”. Then, the electric charge stored in  $C_1$  is discharged and the output of  $A_1$  increases linearly by the Miller effect. The output of  $N_4$  becomes a low level when the output of  $A_1$  reaches to the positive threshold voltage of the Schmitt-trigger circuit  $V_H$ . By this operation,  $M_1$  is turned “OFF”,  $C_1$  is charged, and the output of  $A_1$  decreases linearly by the Miller effect. When the output of  $A_1$  reaches to the negative threshold voltage  $V_L$ , the

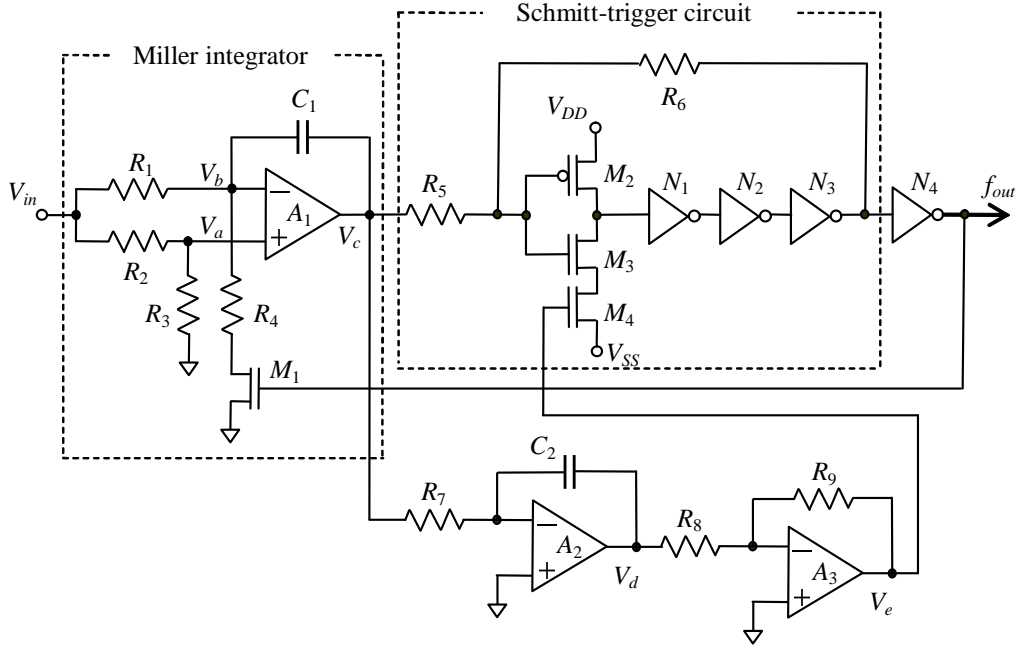


FIGURE 4. Circuit configuration of the proposed VCO

output turns over again and returns to the original state. The proposed VCO performs the oscillating operation by repeating these operations.

**3.2. Relation between the control voltage and the oscillating frequency.** The operation of the part of the Miller integrator is described. In the Miller integrator, we design the resistances  $R_1$ - $R_4$  to satisfy  $R_1 = 2R_4$  and  $R_2 = R_3$ . First,  $V_a$  and  $V_b$  are treated as imaginary short, and expressed as:

$$V_a = V_b. \quad (1)$$

From  $R_2 = R_3$ ,  $V_a$  is expressed as follows.

$$V_a = \frac{1}{2}V_{in}. \quad (2)$$

When the MOS transistor  $M_1$  is “OFF”, the current which flows into  $C_1$ ,  $I_C$ , is given by:

$$I_C = \frac{V_{in} - V_a}{R_1} = \frac{V_{in} - \frac{1}{2}V_{in}}{R_1} = \frac{V_{in}}{2R_1}. \quad (3)$$

On the other hand, when the MOS transistor is “ON”, the current  $I_C$  is given by:

$$I_C = \frac{V_{in} - V_a}{R_1} - \frac{V_a}{R_4} = \frac{V_{in} - \frac{1}{2}V_{in}}{R_1} - \frac{V_a}{\frac{1}{2}R_1} = -\frac{V_{in}}{2R_1}. \quad (4)$$

Therefore, the output voltage of the Miller integrator  $V_c$  increases or decreases linearly, because the capacitance  $C_1$  is charged or discharged by the constant current in proportion to the control voltage  $V_{in}$ .

Next, we describe the Schmitt-trigger circuit. In Figure 4, a pair of MOS transistors  $M_2$  and  $M_3$  can be treated as an inverter although the source of  $M_3$  is connected to the drain of  $M_4$  to compensate the threshold voltage. When the threshold voltage of the inverter consisting of  $M_2$  and  $M_3$  is  $V_{th}$ , two threshold voltages of the Schmitt-trigger circuit,  $V_H$  and  $V_L$ , are expressed as:

$$V_H = \frac{R_5 V_{DD}}{R_6} + \left(1 + \frac{R_5}{R_6}\right) V_{th} \quad (5)$$

and

$$V_L = -\frac{R_5 V_{DD}}{R_6} + \left(1 + \frac{R_5}{R_6}\right) V_{th}. \quad (6)$$

Here, let us derive the oscillating frequency  $f_{out}$ . When the output of the Schmitt-trigger circuit becomes a high level, the time of the half period  $t_{w1}$  is expressed as:

$$t_{w1} = \frac{4R_5 R_1 C_1 V_{DD}}{R_6 V_{in}}. \quad (7)$$

Also the oscillating frequency is expressed as:

$$f_{out} = \frac{R_6 V_{in}}{8R_5 R_1 C_1 V_{DD}}, \quad (8)$$

because the half period  $t_{w2}$  can be obtained in the same way. From Equation (8), the oscillating frequency  $f_{out}$  which is proportional to the input voltage  $V_{in}$  can be obtained.

**3.3. Operation of the threshold automatic compensation.** In this subsection, we describe the operation of the threshold automatic compensation. In the threshold automatic compensation,  $V_c$  is the triangular wave which has the DC component with  $(1 + R_6/R_5)V_{th}$  when the threshold voltage of the inverter consisting of  $M_2$  and  $M_3$  is  $V_{th}$ . Therefore, if  $V_{th}$  is negative, the output of the Miller integrator consisting of  $R_7$ ,  $C_2$ , and  $A_2$ ,  $V_d$ , increases. When the  $V_d$  is connected to the inverting amplifier circuit consisting of  $R_8$ ,  $R_9$ , and  $A_3$ , the output voltage  $V_e$  decreases. By inputting  $V_e$  to the gate of  $M_4$ , the threshold voltage  $V_{th}$  of the inverter consisting of  $M_2$  and  $M_3$  increases. Oppositely, if  $V_{th}$  is positive, the output of the Miller integrator  $V_d$  decreases. When the  $V_d$  is connected to the inverting amplifier circuit, the output voltage  $V_e$  increases. By inputting  $V_e$  to the gate of  $M_4$ , the threshold voltage  $V_{th}$  of the inverter consisting of  $M_2$  and  $M_3$  decreases. By these operations, the threshold voltage of the inverter consisting of  $M_2$  and  $M_3$  can be kept at 0V and obtained the triangular wave around 0V.

**4. Experimental Results.** By using the Onsemi-Sanyo 0.8 $\mu$ m CMOS process, we fabricated the following four types of VCOs into an IC chip: 1) The conventional VCO using the Miller integrator and the Schmitt-trigger with an operational amplifier, 2) The conventional VCO using the Schmitt-trigger with CMOS inverters, 3) The conventional VCO with the threshold automatic compensation circuit, and 4) The proposed VCO.

Figure 5 shows the layout of the proposed VCO. In this experiment, in order to set 800kHz maximum frequency and 50% duty cycle, the parameters are determined as follows:  $R_1 = 60\text{k}\Omega$ ,  $R_2\text{-}R_4 = 30\text{k}\Omega$ ,  $R_5 = 10\text{k}\Omega$ ,  $R_6 = 20\text{k}\Omega$ ,  $R_7 = 600\text{k}\Omega$ ,  $R_8 = 30\text{k}\Omega$ ,  $R_9 = 30\text{k}\Omega$ ,  $C_1 = 5\text{pF}$ , and  $C_2 = 40\text{pF}$ . Also the supply voltage  $V_{DD}$  and  $V_{SS}$  are set to 2.5V and  $-2.5\text{V}$ , respectively. Figure 6(a) shows the measured outputs when the control

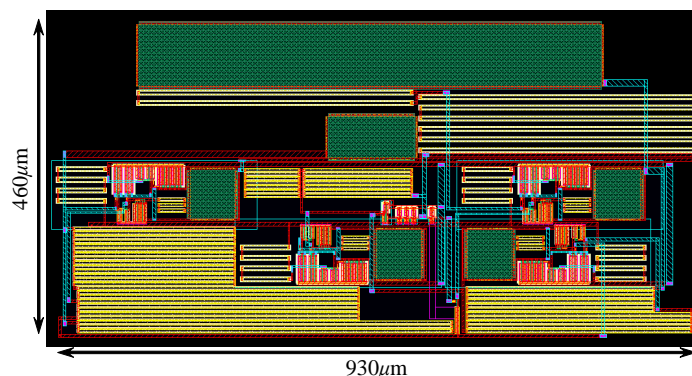


FIGURE 5. Layout of the proposed VCO

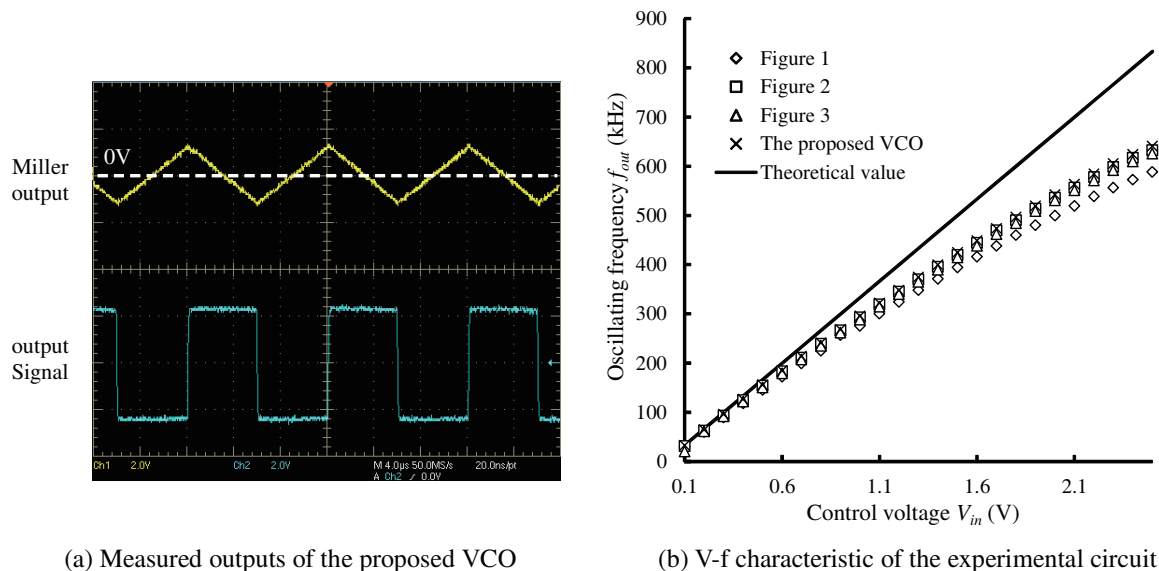


FIGURE 6. Experimental results of the proposed VCO

voltage  $V_{in}$  was set to 1.0V. From this figure, the validity of the circuit design can be confirmed.

Figure 6(b) shows the measured V-f characteristic of the experimental circuits when the control voltage is varied from 0V to 2.5V. From this figure, we can confirm that the proposed VCO shows good linearity although the V-f characteristic is slightly affected by the gate transit time. Also, the conventional circuit of Figure 3 has a problem that source voltage of the CMOS inverter of the n-MOS transistor varies, because the source terminal is connected to the operational amplifier. However, since the variation of the source voltage does not affect the proposed circuit by connecting the source terminal of the n-MOS transistor to  $V_{SS}$ , it is possible to achieve a stable operation.

**5. Conclusion.** In this paper, we proposed a novel VCO using a threshold automatic compensation circuit. Owing to the Schmitt-trigger circuit with CMOS inverters, the proposed circuit showed a good V-f characteristic even if the oscillating frequency is high. Furthermore, the triangular wave around 0V was realized by the threshold automatic compensation circuit.

We fabricated the IC chip of the proposed VCO using the Onsemi-Sanyo  $0.8\mu\text{m}$  CMOS process, and confirmed the circuit design through the experiments using the fabricated IC chip. In the experiment, the V-f characteristic of the proposed circuit showed better linearity than that of the conventional circuits.

In future work, we are going to plan to more improve the linearity of V-f characteristic of the proposed circuit.

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